



Experimental determination of the phase equilibria in the Co–Fe–Zr ternary system

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ARTICLE INFO

Article history:

Received 18 October 2010

Received in revised form

30 December 2010

Accepted 4 January 2011

Available online 13 January 2011

Keywords:

Metal and alloys

Phase diagrams

X-ray diffraction

ABSTRACT

The phase equilibria in the Co–Fe–Zr ternary system were investigated by means of optical microscopy (OM), electron probe microanalysis (EPMA), X-ray diffraction (XRD), and differential scanning calorimetry (DSC) on equilibrated ternary alloys. Four isothermal sections of the Co–Fe–Zr ternary system at 1300 °C, 1200 °C, 1100 °C and 1000 °C were experimentally established. The experimental results indicate that (1) no ternary compound was found in this system; (2) the solubility of Fe in the liquid phase of the Co-rich corner at 1300 °C is extremely large; (3) the liquid phase in the Zr-rich corner and the (Co,Fe)₂Zr phase form the continuous solid solutions from the Co–Zr side to the Fe–Zr side; (4) the solubility of Zr in the fcc (Co, Fe) phase is extremely small.

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1. Introduction

The Co–Fe base alloys are important magnetic materials in applications of electronic industry, information technology and recording media [1,2]. The Co–Fe–Zr system is one of important subsystems for the typical magnetic metallic materials. In addition, the Co–Fe–Zr base alloys are also used as high temperature materials and amorphous materials [3–5]. For the advanced development of high-performance Co–Fe–Zr base alloys, accurate information on the phase equilibria in the Co–Fe–Zr system is especially required. Although the isothermal sections at 500 °C investigated by Mishenina et al. [6] and at 1000 °C determined by Raghavan [7] were available, however, there are still two main conflicts in the isothermal section at 1000 °C (shown in Fig. 1), which are summarized as follows: (1) the existence of the FeZr₂ phase at 1000 °C is obviously not in accordance with that in the Fe–Zr binary phase diagram (presented in Fig. 2) reviewed by Okamoto [8] and (2) the chemical compositions of the Fe₃Zr phase has a big difference from that in Ref. [8]. Therefore, it is important and necessary to comprehensively determine the phase equilibria in the Co–Fe–Zr ternary system.

In the Co–Fe–Zr ternary system, the Co–Fe [9], Co–Zr [10–12] and Fe–Zr [8] three sub-binary systems have been experimentally investigated. The Co–Fe phase diagram is characterized by an extremely narrow solidification range. The fcc continuous solid

solution exists from the fcc (Fe) phase to the fcc (Co) phase over a wide range of temperature [9]. In the Co–Zr phase diagram, there are five intermediate phases: Co₁₁Zr₂, Co₂₃Zr₆, Co₂Zr, CoZr and CoZr₂ [10]. Later, Bataleva et al. [11] confirmed the existence of the CoZr₃ phase. Among these, Co₂Zr and CoZr₃ phases have a range of homogeneity. The main information of the Co–Zr phase diagram is obtained by Pechin et al. [10] and our work [12]. The Fe–Zr system reviewed by Okamoto [8] shows that the stable phases are the liquid phase, terminal solid solutions δFe, αFe, γFe, βZr, and αZr, and four intermetallic compounds, namely, Fe₂₃Zr₆, Fe₂Zr, FeZr₂, and FeZr₃ phases. Nine invariant reactions exist in the system involving all the phases mentioned above. The phase diagram in the Co–Fe [9], Co–Zr [10] and Fe–Zr [8] three sub-binary systems are shown in Fig. 2. The information of the stable solid phases in the three binary systems mentioned above is summarized in Table 1.

Recently, our group has been focused on developing a thermodynamic database of the phase diagrams in the Co-based alloys [13–21]. In order to obtain the detailed information of phase equilibria for the thermodynamic assessment, the objective of the present work is to experimentally determine the isothermal sections at 1300 °C, 1200 °C, 1100 °C and 1000 °C using the equilibrated ternary alloys, which will meet the need for the thermodynamic description of the Co–Fe–Zr ternary system and provide a better understanding of microstructures of promising alloys for practical applications.

2. Experimental procedure

Cobalt (99.8 wt.%), iron (99.9 wt.%) and zirconium (99.7 wt.%) were used as starting materials. Bulk buttons were prepared from pure elements by arc melting under

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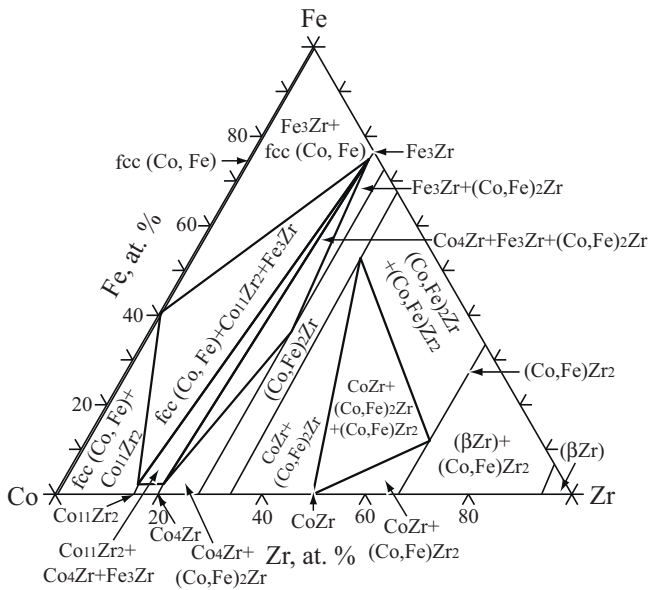


Fig. 1. The isothermal section of the Co–Fe–Zr system at 1000 °C reviewed by Raghavan [7].

high purity argon atmosphere using a non-consumable tungsten electrode. The ingots were melted at least five times in order to achieve their homogeneity. The sample weight is around 20 g and the weight loss during melting is generally less than 0.20% of the sample weight. Afterwards, the ingots were cut into small pieces for heat treatments and further observations.

The specimens were wrapped in Mo foil in order to prevent direct contact with the quartz ampoule, and put into quartz evacuated and backfilled with argon gas. The specimens were annealed in temperature range between 1000 °C and 1300 °C, respectively. The time of the heat treatment varied from several hours to 3 months depending on temperature and composition of the specimen. At the end of the heat treatment, the specimens were quenched into ice water.

After standard metallographic preparation, the microstructural observations were carried out by optical microscopy (OM) and scanning electron microscopy

(SEM). The reliable equilibrium compositions of each phase were determined by electron probe microanalysis (EPMA) (JXA-8100R, JEOL, Japan) based on the wavelength dispersive spectroscopy (WDS) and pure elements cobalt, iron and zirconium were used as standard materials. The conditions of measurements were 20.0 kV for voltage and 10 nA for beam current, respectively. The equilibrium compositions were obtained by averaging the compositions determined by EPMA.

The X-ray diffraction (XRD) was used to identify the crystal structure of the constituent phases. The X-ray powder diffraction patterns of the experimental samples were carried out on a Phillips Analytical X-pert diffractometer using Cu K α radiation at 40 kV and 30 mA. The data were collected in the range of 2 θ from 20° to 90° at a step width of 0.0167°. The differential scanning calorimetry (DSC) method was used to determine the temperature of phase transformation. Al₂O₃ power was used as reference substance. The heating and cooling rates were both set to 10 °C/min. All measurements were conducted under argon atmosphere.

3. Results and discussion

3.1. Microstructure

The BSE (back-scattered electron) images of the typical ternary alloys for the Co–Fe–Zr system are presented in Fig. 3(a)–(h). Phase identification was based on equilibrium composition measured by EPMA. The Co₈₀Fe₁₃Zr₇ (at.%) and Co₅₀Fe₁₀Zr₄₀ (at.%) alloys annealed at 1300 °C for 1 h and 6 days are respectively located in the two-phase regions (liquid + fcc (Co, Fe)) and (CoZr + (Co,Fe)₂Zr), as characterized in Fig. 3(a) and (b), respectively. The fcc (Co, Fe) phase and the (Co,Fe)₂Zr phase distribute in the matrix of the liquid phase and CoZr phase, respectively. In the Co₈₇Fe₆Zr₇ (at.%) alloy quenched from 1200 °C, the two phases Co₁₁Zr₂ and fcc (Co, Fe) were identified, as shown in Fig. 3(c). The three-phase equilibrium of the liquid + (Co,Fe)₂Zr + CoZr were identified in the Co₃₀Fe₂₀Zr₅₀ (at.%) alloys quenched from 1200 °C for 6 h, as indicated in Fig. 3(d). The Co₄₀Fe₄₅Zr₁₅ (at.%) and Co₃₅Fe₃Zr₆₂ (at.%) annealed at 1100 °C for 3 months are located in the three-phase region of the Fe₂₃Zr₆ + fcc (Co, Fe) + (Co,Fe)₂Zr and two-phase region of the CoZr + CoZr₂, as shown in Fig. 3(e–f). In addition, the two-phase equilibrium of the (Co,Fe)₂Zr + CoZr₂ and three-phase equilibrium of the CoZr₂ + (Co,Fe)₂Zr + CoZr were identified

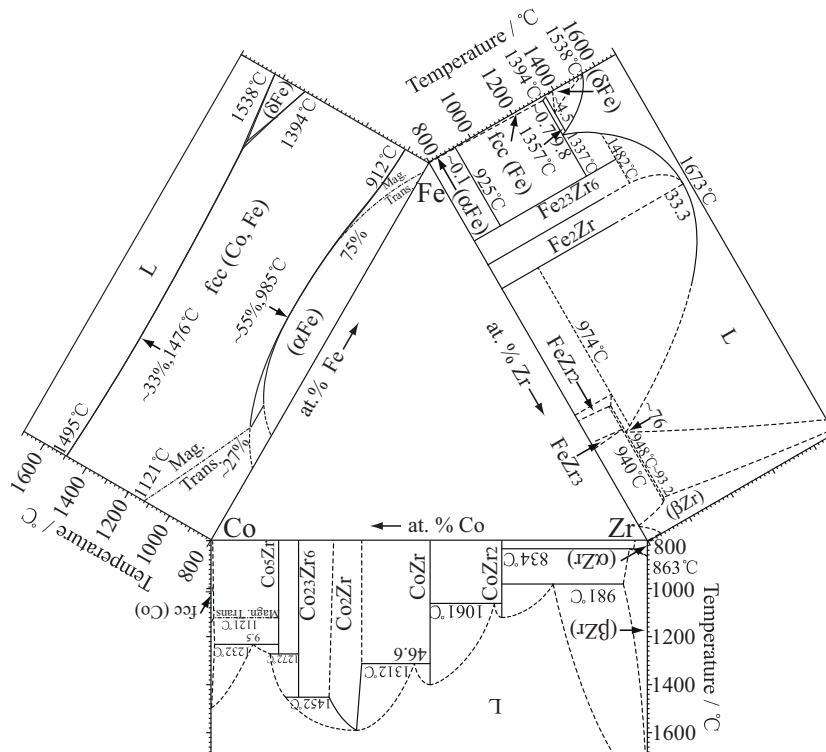


Fig. 2. Binary phase diagrams constituting the Co–Fe–Zr ternary system [8–10].

Table 1
The stable phases in the three binary systems.

System	Phase	Pearson's symbol	Prototype	Strukturbericht	References
Co–Fe	fcc (Co, Fe)	cF4	Cu	A1	[8]
	(α Fe)	c12	W	A2	[8]
	(δ Fe)	c12	W	A2	[8]
Co–Zr	fcc (Co)	cF4	Cu	A1	[9]
	(ϵ Co)	hP2	Mg	A3	[9]
	Co ₂₃ Zr ₆	cF116	Mn ₂₃ Th ₆	D8 ₂	[9]
	Co ₂ Zr	cF24	Cu ₂ Mg	C15	[9]
	CoZr	cP2	CsCl	B2	[9]
	CoZr ₂	Ti12	Al ₂ Cu	C16	[9]
	(β Zr)	C12	W	A2	[9]
	(α Zr)	hP2	Mg	A3	[9]
	CoZr ₃	oC16	Re ₃ B	E1 ₁₂	[9]
	Fe–Zr	(α Zr)	hP2	Mg	A3
(β Zr)		C12	W	A2	[12]
FeZr ₃		oC16	Re ₃ B	E1 ₁₂	[12]
FeZr ₂		Ti12	Al ₂ Cu	C16	[12]
Fe ₂ Zr		cF24	Cu ₂ Mg	C15	[12]
Fe ₂₃ Zr ₆		cF116	Mn ₂₃ Th ₆	D8 ₂	[12]
(α Fe)		c12	W	A2	[12]
fcc (Fe)		cF4	Cu	A1	[12]
(δ Fe)		c12	W	A2	[12]

in the Co₁₂Fe₃₈Zr₅₀ (at.%) and Co₂₅Fe₃₀Zr₄₅ (at.%) alloys annealed at 1000 °C for 4 months, respectively, and indicated in Fig. 3(g) and (h), respectively.

3.2. Structure and melting points

The Co₅₀Fe₁₀Zr₄₀ (at.%) alloy annealed at 1300 °C for 6 days was substantiated by the XRD experiment, as shown in Fig. 4(a), where the characteristic peaks of the (Co,Fe)₂Zr and CoZr phases are well distinguished by different symbols, which are consistent with the results determined by EPMA, as shown in Fig. 3(b). In addition, the XRD result of Co₂₅Fe₃₀Zr₄₅ (at.%) alloy quenched from 1000 °C is shown in Fig. 4(b), where the characteristic peaks of the CoZr, CoZr₂ and (Co,Fe)₂Zr were marked by different symbols, which is observed in Fig. 3(h).

The DSC analysis was performed in order to determined the melting points of three different alloys Co₆Fe₁₉Zr₇₅ (at.%), Co₁₂Fe₁₃Zr₇₅ (at.%) and Co₁₉Fe₆Zr₇₅ (at.%). Their DSC curves on heating are presented in Fig. 5, respectively. It can be known that the appearance of the liquid phase in the Zr-rich corner is below 1000 °C, which indicates that there should be a liquid phase from Co–Zr side to Fe–Zr side at 1000 °C.

3.3. Isothermal section

The equilibrium compositions of the Co–Fe–Zr ternary system at 1300 °C, 1200 °C, 1100 °C and 1000 °C determined by EPMA are listed in Tables 2–5, respectively.

Based on these experimental data mentioned above, the isothermal sections at 1300 °C, 1200 °C, 1100 °C and 1000 °C were

Table 2
Equilibrium compositions of the Co–Fe–Zr system at 1300 °C.

Alloy (at.%)	Equilibria Phase 1/phase 2/phase 3	Composition (at.%)					
		Phase 1		Phase 2		Phase 3	
		Fe	Zr	Fe	Zr	Fe	Zr
Co ₄₀ Fe ₁₀ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr/liquid	24.09	32.61	9.32	48.55		12.39
Co ₄₀ Fe ₂₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	26.45	32.29	5.08	48.78		
Co ₄₀ Fe ₃₅ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	40.83	20.19	33.60	25.49		
Co ₄₀ Fe ₄₅ Zr ₁₅	Liquid/Fe ₂₃ Zr ₆	51.98	8.54	38.82	20.33		
Co ₆₀ Fe ₃₀ Zr ₁₀	fcc (Co, Fe)/liquid	40.35	2.17	27.58	10.19		
Co ₆₀ Fe ₂₁ Zr ₁₉	Liquid/Co ₂₃ Zr ₆	28.14	9.89	20.19	19.72		
Co ₆₀ Fe ₁₅ Zr ₂₅	Co ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	16.92	21.23	13.57	25.58		
Co ₁₀ Fe ₈₀ Zr ₁₀	fcc (Co, Fe)/Fe ₂₃ Zr ₆	89.50	0.14	66.78	19.81		
Co ₅₀ Fe ₄₀ Zr ₁₀	fcc (Co, Fe)/liquid	50.19	0.35	36.97	10.33		
Co ₆₅ Fe ₂₃ Zr ₁₂	Liquid/Co ₂₃ Zr ₆	23.89	10.97	13.64	20.54		
Co ₈₀ Fe ₁₃ Zr ₇	fcc (Co, Fe)/liquid	14.10	0.02	7.79	10.04		
Co ₈₇ Fe ₆ Zr ₇	fcc (Co, Fe)/liquid	8.05	0.14	4.85	9.16		
Co ₇ Fe ₄₃ Zr ₅₀	(Co,Fe) ₂ Zr/liquid	63.04	31.71	24.20	65.23		
Co ₁₂ Fe ₃₈ Zr ₅₀	(Co,Fe) ₂ Zr/liquid	58.14	32.24	18.91	65.13		
Co ₂₅ Fe ₃₀ Zr ₄₅	(Co,Fe) ₂ Zr/CoZr/liquid	42.77	33.57	10.46	49.95	12.45	64.58
Co ₃₀ Fe ₂₀ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr/liquid	40.39	32.46	9.69	48.96	13.09	63.20
Co ₅₀ Fe ₁₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	12.45	32.26	2.38	49.18		
Co ₅₅ Fe ₅ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	8.02	32.31	1.05	49.03		
Co ₃₅ Fe ₃ Zr ₆₂	CoZr/liquid	2.89	48.61	3.92	65.43		
Co ₇₀ Fe ₅ Zr ₂₅	Co ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	6.59	20.24	3.78	25.49		
Co ₃₅ Fe ₄₀ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	46.42	20.21	39.70	25.39		
Co ₇ Fe ₆₈ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	73.14	20.23	67.88	25.45		
Co _{6,7} Fe _{3,3} Zr ₉₀	Liquid/(β Zr)	1.76	84.41	0.20	97.00		
Co _{3,3} Fe _{6,7} Zr ₉₀	Liquid/(β Zr)	9.67	83.76	2.63	96.76		

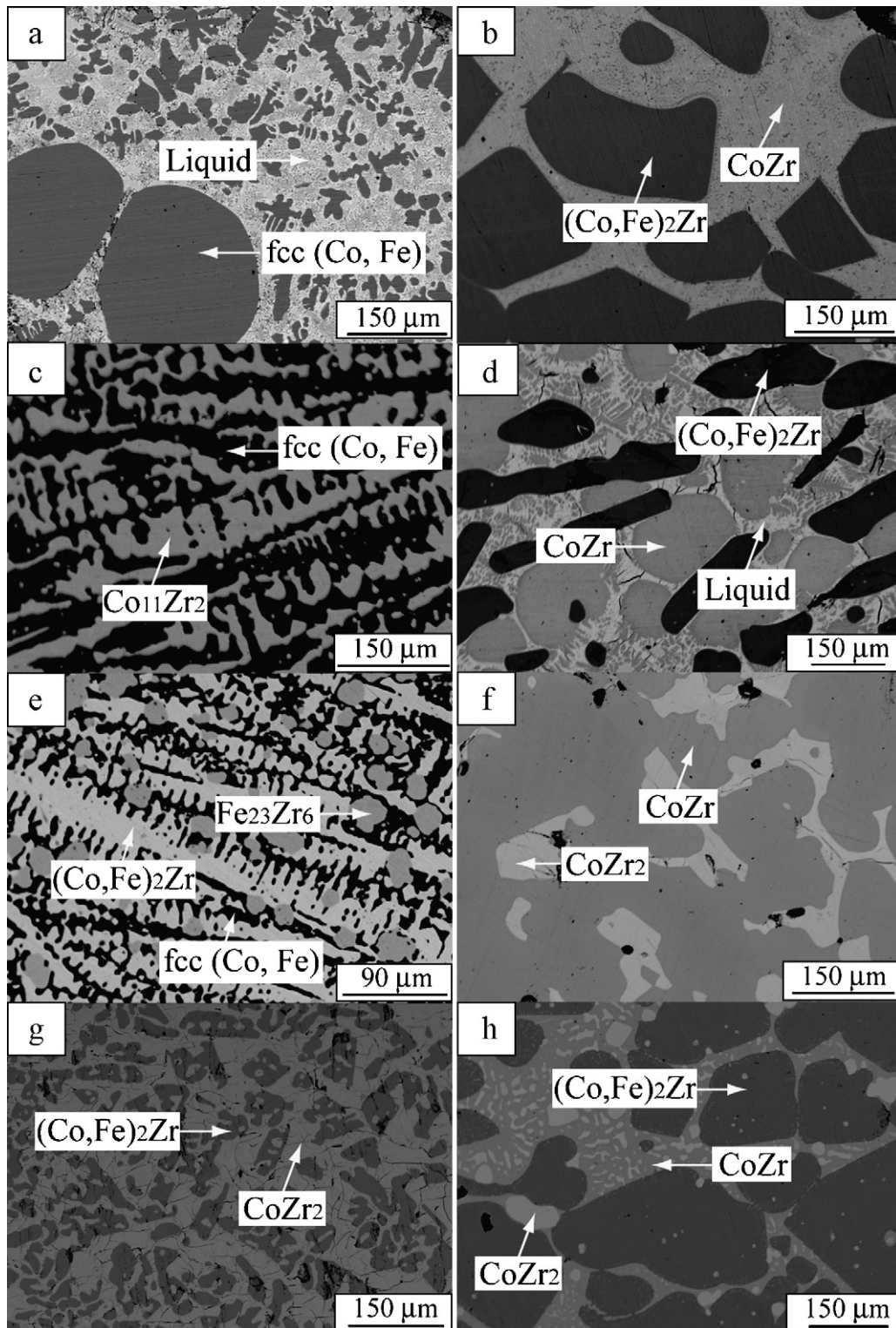


Fig. 3. BSE images of typical ternary alloys: (a) $\text{Co}_{80}\text{Fe}_{13}\text{Zr}_7$ (at.%) alloy annealed at 1300°C for 1 h; (b) $\text{Co}_{50}\text{Fe}_{10}\text{Zr}_{40}$ (at.%) alloy annealed at 1300°C for 6 days; (c) $\text{Co}_{87}\text{Fe}_6\text{Zr}_7$ (at.%) alloy annealed at 1200°C for 1 month; (d) $\text{Co}_{30}\text{Fe}_{20}\text{Zr}_{50}$ (at.%) alloy annealed at 1200°C for 6 h; (e) $\text{Co}_{40}\text{Fe}_{45}\text{Zr}_{15}$ (at.%) alloy annealed at 1100°C for 3 months; (f) $\text{Co}_{35}\text{Fe}_3\text{Zr}_{62}$ (at.%) alloy annealed at 1100°C for 3 months; (g) $\text{Co}_{12}\text{Fe}_{38}\text{Zr}_{50}$ (at.%) alloy annealed at 1000°C for 4 months; (h) $\text{Co}_{25}\text{Fe}_{30}\text{Zr}_{45}$ (at.%) alloy annealed at 1000°C for 4 months.

constructed in Fig. 6(a)–(d). Fig. 6(a) shows the isothermal section at 1300°C , where the solubility of Zr in the fcc (Co, Fe) phase is extremely small and the solubility of Fe in liquid phase of the Co-rich corner is extremely large. In addition, the liquid phase in the Zr-rich corner and the $(\text{Co,Fe})_2\text{Zr}$ phase form the contin-

uous solid solutions from the Co–Zr side to the Fe–Zr side. The three-phase equilibrium $(\text{CoZr} + (\text{Co,Fe})_2\text{Zr} + \text{liquid})$, rather than ternary compound was identified. Three three-phase equilibria, fcc (Co, Fe) + liquid + $\text{Fe}_{23}\text{Zr}_6$, liquid + $(\text{Co,Fe})_2\text{Zr} + \text{Fe}_{23}\text{Zr}_6$ and liquid + $(\text{Co,Fe})_2\text{Zr} + \text{Co}_{23}\text{Zr}_6$, as shown in Fig. 5(a) in dashed lines, were

Table 3
Equilibrium compositions of the Co–Fe–Zr system at 1200 °C.

Alloy (at.%)	Equilibria Phase 1/phase 2/phase 3	Composition (at.%)					
		Phase 1		Phase 2		Phase 3	
		Fe	Zr	Fe	Zr	Fe	Zr
Co ₄₀ Fe ₁₀ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr/Liquid	40.25	32.47	8.75	48.58	13.56	65.07
Co ₄₀ Fe ₂₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	28.67	32.54	4.75	49.10		
Co ₄₀ Fe ₃₅ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	40.55	19.92	33.83	25.37		
Co ₄₀ Fe ₄₅ Zr ₁₅	fcc (Co, Fe)/Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	61.83	0.26	38.06	19.65	32.37	23.66
Co ₆₀ Fe ₃₀ Zr ₁₀	fcc (Co, Fe)/Co ₂₃ Zr ₆	37.20	0.07	19.23	20.24		
Co ₆₀ Fe ₂₁ Zr ₁₉	fcc (Co, Fe)/Co ₂₃ Zr ₆	35.49	0.39	18.20	20.61		
Co ₆₀ Fe ₁₅ Zr ₂₅	Co ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	19.10	20.19	14.61	25.82		
Co ₁₀ Fe ₈₀ Zr ₁₀	fcc (Co, Fe)/Fe ₂₃ Zr ₆	90.18	0.06	66.16	20.68		
Co ₂₀ Fe ₇₀ Zr ₁₀	fcc (Co, Fe)/Fe ₂₃ Zr ₆	80.23	0.03	47.85	20.03		
Co ₃₀ Fe ₆₃ Zr ₇	fcc (Co, Fe)/Fe ₂₃ Zr ₆	70.55	0.07	43.12	20.76		
Co ₅₀ Fe ₄₀ Zr ₁₀	fcc (Co, Fe)/(Co,Fe) ₂ Zr	47.23	0.08	17.54	24.08		
Co ₆₅ Fe ₂₃ Zr ₁₂	fcc (Co, Fe)/Co ₂₃ Zr ₆	28.60	0.05	13.82	20.13		
Co ₈₀ Fe ₁₃ Zr ₇	fcc (Co, Fe)/Co ₁₁ Zr ₂	15.42	0.01	6.24	15.26		
Co ₈₇ Fe ₆ Zr ₇	fcc (Co, Fe)/Co ₁₁ Zr ₂	6.55	0.13	2.54	15.18		
Co ₇ Fe ₄₃ Zr ₅₀	(Co,Fe) ₂ Zr/liquid	62.78	32.63	23.21	66.98		
Co ₁₂ Fe ₃₈ Zr ₅₀	(Co,Fe) ₂ Zr/liquid	58.57	31.62	19.64	64.73		
Co ₂₅ Fe ₃₀ Zr ₄₅	(Co,Fe) ₂ Zr/CoZr/liquid	41.69	31.60	9.09	49.75	13.87	65.93
Co ₃₀ Fe ₂₀ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr/liquid	40.72	31.83	8.56	48.15	13.99	64.35
Co ₅₀ Fe ₁₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	15.13	31.45	1.77	48.60		
Co ₅₅ Fe ₅ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	7.37	32.41	0.74	49.08		
Co ₃₅ Fe ₃ Zr ₆₂	CoZr/liquid	2.91	48.87	3.87	63.82		
Co ₇₀ Fe ₅ Zr ₂₅	Co ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	5.43	20.75	4.11	24.24		
Co ₃₅ Fe ₄₀ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	41.95	20.14	37.06	25.27		
Co ₇ Fe ₆₈ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	73.05	20.24	66.63	25.50		
Co ₇₀ Fe ₁₁ Zr ₁₉	Co ₁₁ Zr ₂ /Co ₂₃ Zr ₆	10.71	15.38	9.95	20.00		
Co _{6,7} Fe _{3,3} Zr ₉₀	Liquid/(βZr)	6.76	76.24	1.12	96.76		
Co _{3,3} Fe _{6,7} Zr ₉₀	Liquid/(βZr)	15.30	78.16	2.35	96.09		

still not determined. In the isothermal section at 1200 °C (Fig. 6(b)), two three-phase equilibria, CoZr + (Co,Fe)₂Zr + liquid and fcc (Co, Fe) + (Co,Fe)₂Zr + Fe₂₃Zr₆ were determined. The solubility of Zr in the Co₂₃Zr₆ phase is larger than that in the Co₁₁Zr₂ phase. The liquid phase in the Co-rich corner disappears, but the liquid phase in the Zr-rich corner still form the continuous solid solutions from

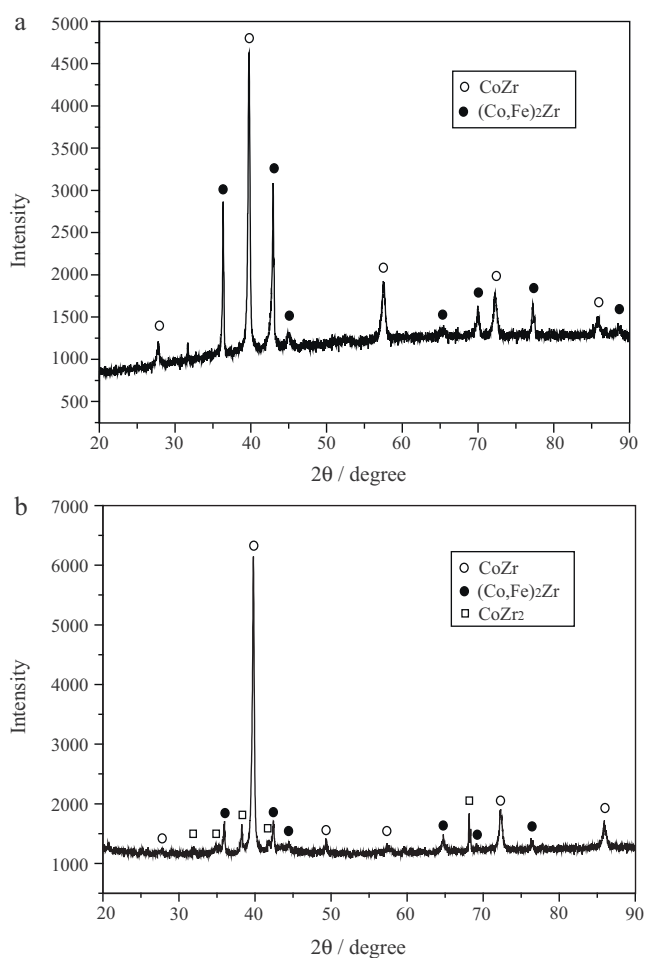
the Co–Zr side to the Fe–Zr side. As shown in Fig. 6(c), the solid CoZr₂ phase, existing only below 1200 °C in the Co–Zr binary system [10–12], appears in the isothermal section at 1100 °C. The solubility of Fe in the CoZr₂ phase was found to be extremely large. Three three-phase equilibria, CoZr + (Co,Fe)₂Zr + CoZr₂, fcc (Co, Fe) + (Co,Fe)₂Zr + Fe₂₃Zr₆ and fcc (Co, Fe) + Co₁₁Zr₂ + Co₂₃Zr₆

Table 4
Equilibrium compositions of the Co–Fe–Zr system at 1100 °C.

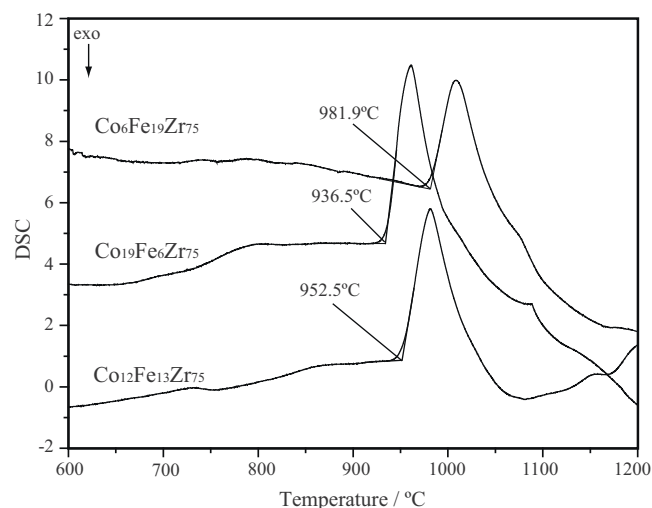
Alloy (at.%)	Equilibria Phase 1/phase 2/phase 3	Composition (at.%)					
		Phase 1		Phase 2		Phase 3	
		Fe	Zr	Fe	Zr	Fe	Zr
Co ₄₀ Fe ₁₀ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr	32.17	34.32	5.66	50.54		
Co ₄₀ Fe ₂₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	28.85	32.84	4.32	49.01		
Co ₄₀ Fe ₃₅ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	38.42	19.16	31.95	25.22		
Co ₄₀ Fe ₄₅ Zr ₁₅	fcc (Co, Fe)/Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	61.39	0.08	37.07	19.70	31.67	23.35
Co ₆₀ Fe ₃₀ Zr ₁₀	fcc (Co, Fe)/Co ₂₃ Zr ₆	40.45	0.48	18.73	20.32		
Co ₆₀ Fe ₂₁ Zr ₁₉	fcc (Co, Fe)/Co ₂₃ Zr ₆	38.11	0.30	16.49	20.25		
Co ₆₀ Fe ₁₅ Zr ₂₅	Co ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	20.45	20.04	14.91	25.35		
Co ₁₀ Fe ₈₀ Zr ₁₀	fcc (Co, Fe)/Fe ₂₃ Zr ₆	90.43	0.69	62.02	20.39		
Co ₂₀ Fe ₇₀ Zr ₁₀	fcc (Co, Fe)/Fe ₂₃ Zr ₆	81.97	0.41	50.17	20.65		
Co ₃₀ Fe ₆₃ Zr ₇	fcc (Co, Fe)/Fe ₂₃ Zr ₆	70.51	0.19	43.08	20.37		
Co ₅₀ Fe ₄₀ Zr ₁₀	fcc (Co, Fe)/(Co,Fe) ₂ Zr	49.95	0.33	22.30	23.15		
Co ₆₅ Fe ₂₃ Zr ₁₂	fcc (Co, Fe)/Co ₂₃ Zr ₆	32.68	0.11	11.51	20.05		
Co ₈₀ Fe ₁₃ Zr ₇	fcc (Co, Fe)/Co ₁₁ Zr ₂	17.02	0.12	6.88	15.24		
Co ₈₇ Fe ₆ Zr ₇	fcc (Co, Fe)/Co ₁₁ Zr ₂	7.79	0.04	2.80	15.34		
Co ₇ Fe ₄₃ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr ₂	62.75	31.52	22.67	65.45		
Co ₁₂ Fe ₃₈ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr ₂	58.59	32.14	20.02	63.75		
Co ₂₅ Fe ₃₀ Zr ₄₅	(Co,Fe) ₂ Zr/CoZr/CoZr ₂	50.41	30.72	12.54	48.18	15.15	62.14
Co ₃₀ Fe ₂₀ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr/CoZr ₂	50.87	31.05	13.06	48.16	15.65	63.15
Co ₅₀ Fe ₁₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	15.15	32.08	1.61	48.29		
Co ₅₅ Fe ₅ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	7.75	31.48	0.82	48.41		
Co ₃₅ Fe ₃ Zr ₆₂	CoZr/CoZr ₂	2.91	48.25	3.20	68.51		
Co _{72,5} Fe _{7,5} Zr ₂₀	Co ₁₁ Zr ₂ /Co ₂₃ Zr ₆	7.79	15.34	4.62	21.05		
Co ₃₅ Fe ₄₀ Zr ₂₅	fcc (Co, Fe)/(Co,Fe) ₂ Zr	45.58	19.51	38.63	25.39		
Co ₇ Fe ₆₈ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	73.90	18.96	67.08	25.14		
Co ₇₀ Fe ₁₁ Zr ₁₉	fcc (Co, Fe)/Co ₁₁ Zr ₂ /Co ₂₃ Zr ₆	20.74	1.49	11.08	15.01	7.39	20.97
Co _{6,7} Fe _{3,3} Zr ₉₀	Liquid/(βZr)	7.71	75.58	13.37	96.75		
Co _{3,3} Fe _{6,7} Zr ₉₀	Liquid/(βZr)	19.10	75.24	0.13	97.82		

Table 5
Equilibrium compositions of the Co–Fe–Zr system at 1000 °C.

Alloy (at.%)	Equilibria Phase 1/phase 2/phase 3	Composition (at.%)					
		Phase 1		Phase 2		Phase 3	
		Fe	Zr	Fe	Zr	Fe	Zr
Co ₄₀ Fe ₁₀ Zr ₅₀	CoZr/CoZr ₂	9.29	48.72	12.44	64.02		
Co ₄₀ Fe ₂₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	28.73	32.67	4.01	49.52		
Co ₄₀ Fe ₃₅ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	41.49	20.83	33.36	26.17		
Co ₄₀ Fe ₄₅ Zr ₁₅	fcc (Co, Fe)/Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	63.45	0.26	38.33	20.40	30.97	23.94
Co ₆₀ Fe ₃₀ Zr ₁₀	fcc (Co, Fe)/Co ₂₃ Zr ₆	40.34	0.38	18.57	20.34		
Co ₆₀ Fe ₁₅ Zr ₂₅	Co ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	20.35	19.94	14.76	24.06		
Co ₁₀ Fe ₈₀ Zr ₁₀	fcc (Co, Fe)/Fe ₂₃ Zr ₆	90.91	0.11	66.39	20.81		
Co ₂₀ Fe ₇₀ Zr ₁₀	fcc (Co, Fe)/Fe ₂₃ Zr ₆	80.85	0.22	53.07	20.99		
Co ₃₀ Fe ₆₃ Zr ₇	fcc (Co, Fe)/Fe ₂₃ Zr ₆	70.02	0.24	42.77	20.24		
Co ₅₀ Fe ₄₀ Zr ₁₀	fcc (Co, Fe)/(Co,Fe) ₂ Zr	48.86	0.17	20.45	24.28		
Co ₆₅ Fe ₂₃ Zr ₁₂	fcc (Co, Fe)/Co ₂₃ Zr ₆	32.77	0.89	11.11	21.25		
Co ₈₀ Fe ₁₃ Zr ₇	fcc (Co, Fe)/Co ₂₃ Zr ₆	15.81	0.08	4.83	19.19		
Co ₈₇ Fe ₆ Zr ₇	fcc (Co, Fe)/Co ₁₁ Zr ₂	7.17	0.04	2.65	15.52		
Co ₇ Fe ₄₃ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr ₂	66.25	29.91	27.71	63.37		
Co ₁₂ Fe ₃₈ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr ₂	62.26	30.35	18.97	64.58		
Co ₂₅ Fe ₃₀ Zr ₄₅	(Co,Fe) ₂ Zr/CoZr/CoZr ₂	43.35	31.85	13.89	49.24	12.98	65.73
Co ₃₀ Fe ₂₀ Zr ₅₀	(Co,Fe) ₂ Zr/CoZr/CoZr ₂	45.18	32.00	14.13	49.33	10.84	65.18
Co ₅₀ Fe ₁₀ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	16.29	32.64	1.50	49.34		
Co ₅₅ Fe ₅ Zr ₄₀	(Co,Fe) ₂ Zr/CoZr	8.82	31.80	7.42	48.69		
Co ₃₅ Fe ₃ Zr ₆₂	CoZr/CoZr ₂	3.65	49.68	2.89	65.79		
Co ₇₀ Fe ₅ Zr ₂₅	Co ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	7.53	21.09	4.77	25.47		
Co ₃₅ Fe ₄₀ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	46.22	19.61	38.60	23.06		
Co ₇ Fe ₆₈ Zr ₂₅	Fe ₂₃ Zr ₆ /(Co,Fe) ₂ Zr	73.67	20.12	66.85	25.29		
Co ₇₀ Fe ₁₁ Zr ₁₉	fcc (Co, Fe)/Co ₂₃ Zr ₆	21.42	0.56	6.73	20.94		
Co _{6.7} Fe _{3.3} Zr ₉₀	Liquid/(βZr)	8.16	75.05	1.75	96.23		
Co _{3.3} Fe _{6.7} Zr ₉₀	Liquid/(βZr)	16.25	75.17	3.27	95.89		

**Fig. 4.** X-ray diffraction patterns obtained from (a) Co₅₀Fe₁₀Zr₄₀ (at.%) alloy annealed at 1300 °C for 6 days and (b) Co₂₅Fe₃₀Zr₄₅ (at.%) alloy annealed at 1000 °C for 4 months.

were determined and three three-phase equilibria shown in dashed line were still not determined. In the isothermal section at 1000 °C (Fig. 6(d)), the liquid phase was found to still exist in the Zr-rich corner and formed the continuous solutions from the Co–Zr side to Fe–Zr side, which also corresponds to the results of DSC analysis mentioned above, showing that the temperature of liquid phase of the Zr-rich corner appears at about 985 °C. The isothermal section at 1000 °C determined in present work is different from 1000 °C investigated by Raghavan [7] (Fig. 1). In the present work, the melting point of the FeZr₂ phase was determined to be about 955.6 °C, which indicated that the FeZr₂ phase does not exist at 1000 °C. Thus, the continuous solid solution of (Co,Fe)Zr₂ phase does not exist at 1000 °C.

**Fig. 5.** DSC heating curves of the Co₆Fe₁₉Zr₇₅ (at.%), Co₁₉Fe₆Zr₇₅ (at.%) and Co₁₂Fe₁₃Zr₇₅ (at.%) alloys.

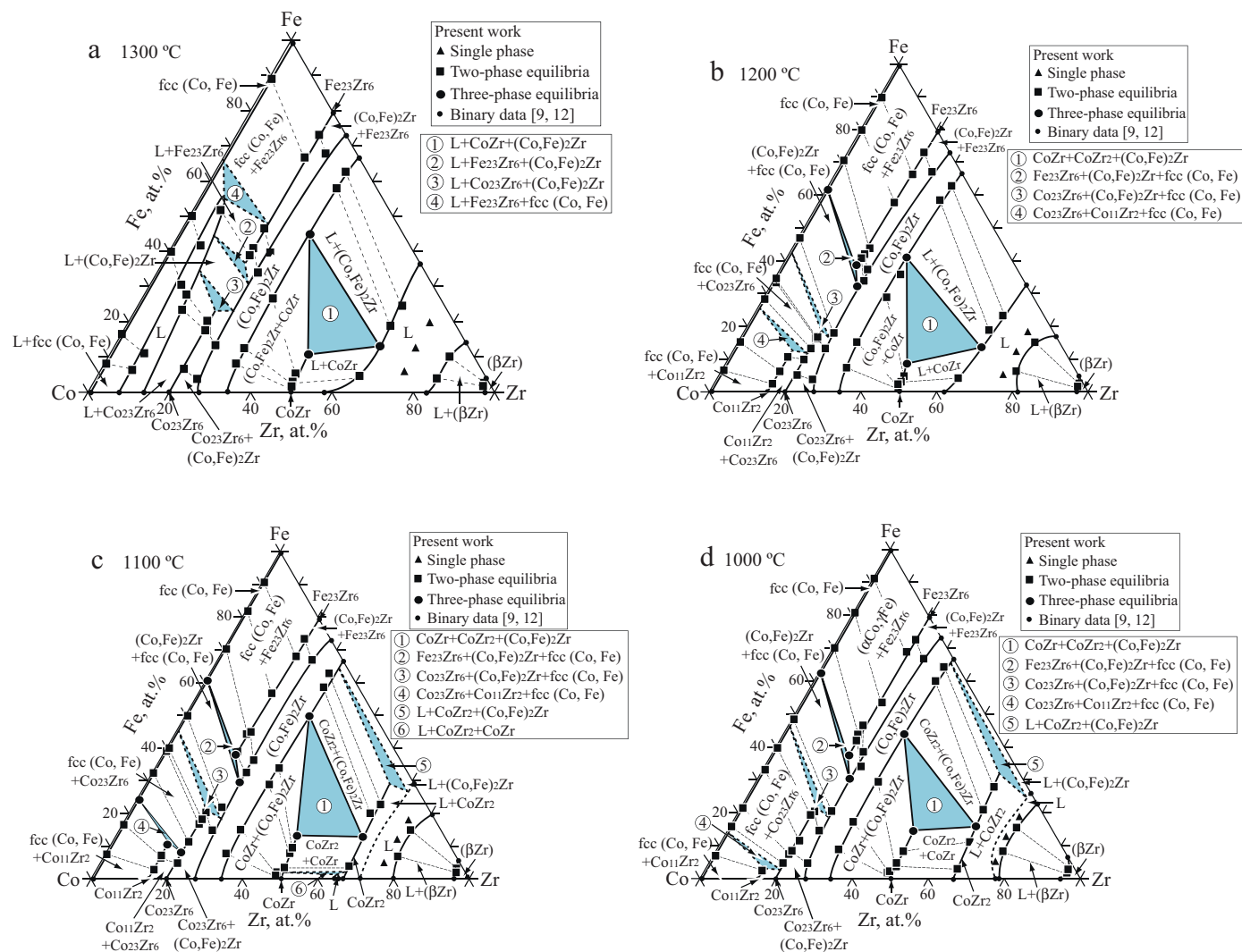


Fig. 6. Experimentally determined isothermal sections of the Co–Fe–Zr system: (a) 1300 °C; (b) 1200 °C; (c) 1100 °C; (d) 1000 °C.

4. Conclusions

Four isothermal sections of the Co–Fe–Zr ternary system at 1300 °C, 1200 °C, 1100 °C and 1000 °C were experimentally determined using equilibrated ternary alloys. The obtained experimental results show that: (1) the solubility of Fe in liquid phase of Co-rich corner at 1300 °C is extremely large; (2) the liquid phase of Zr-rich corner and the (Co,Fe)₂Zr phase form the continuous solid solutions from the Co–Zr side to the Fe–Zr side; (3) the solubility of Zr in fcc (Co, Fe) phase is extremely small; (4) no ternary compound was found in this system.

The newly determined phase equilibria of the Co–Fe–Zr ternary system will provide additional support for the thermodynamic assessment of this system in the underway work and practical application for the amorphous alloys.

Acknowledgements

This work was supported by the National Natural Science Foundation of China (Grant Nos. 51031003, 50771088, 50971109), the Ministry of Science and Technology of China (Grant Nos. 2009DFA52170 and 2009AA03Z101). The Support from Fujian Provincial Department of Science & Technology (Grant No.

2009I0024), Xiamen City Department of Science & Technology (Grant No. 3502Z20093001), and Aviation Science Fund (Grant No. 2009ZF68010) are acknowledged.

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